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(84)

Polyolefin syntactic foams for pipeline insulation use.

(54) An insulating composition comprises a polyolefin, preferably polypropylene, and hollow microspheres, at least some of which have been pre-treated with a chain-scission agent and, optionally, a functionalizing agent for the polyolefin, before addition to the polyolefin melt. The provision of the chain-scission on the microspheres enables the microspheres to be compounded substantially without breakage with low Melt Flow Index polyolefins, with the result that the resultant composite material can be employed in rigorous application areas, for examples as an extruded flowline insulation.

EP 0 473 215 A1

This invention relates to polyolefin/filler composite materials, and their preparation. The invention relates in particular to polyolefin/filler composite materials in which the filler comprises hollow microspheres. Such materials are known as polyolefin "syntactic foams".

The main proposed field of use of the materials of the present invention is thermal insulation, in particular insulation of underwater flowlines. There are onerous requirements on an insulating material for an underwater flowline. Desirably, the material should:

- have a low Melt Flow Index so that it can be extruded in a pipe extrusion process
- be resistant to microsphere breakage during the preparation of the material and subsequent application to a pipe
- permit substantial tensile elongation, to enable a flowline to be installed by any installation method including reel barging
- exhibit low creep over a long period, perhaps a service life of 30 years, during which hot oil may be conveyed within the flowline
- have excellent mechanical properties.

Polyolefin/filler composite materials in which the filler comprises "glass bubbles" are described in Research Disclosure 253015. This article discloses that it is possible to compound "glass bubbles" with inter alia polypropylene using extrusion equipment with less than 5% by weight breakage, to produce low-density composite materials. Proposed uses thereof are extruded parts for buoyancy and thermal insulation and large automotive mouldings.

DE 2445075 describes a film coating in which microspheres are coated with a small amount of polymer, then applied to a support and heated. The polymer may comprise a peroxide e.g. 3-10 parts per 100 parts polymer. The use of polypropylene or polybutylenes is not described or proposed.

When it was attempted, during experimentation, to incorporate microspheres into a polyolefin to make a composite material suitable for rigorous applications such as flowline insulation, it was found to be possible to do so adequately but only using base polypropylenes of high Melt Flow Index (MFI). The resultant composite materials generally had Melt Flow Indexes which were too high for application by the "pipe extrusion" method and/or have unsuitable mechanical properties for flowline insulation. Furthermore, it is known that the creep resistance of materials of high Melt Flow Index is poor. When it was attempted to incorporate microspheres in a base polypropylene of low Melt Flow Index, it was found that a substantial proportion of the microspheres were broken during the compounding or subsequent extrusion, so that the insulation properties were inadequate.

Thus the proposal in Research Disclosure that "glass bubbles" can be compounded with polypropylene and the resultant composite material extruded would only appear to hold good for what might be termed non-rigorous applications.

The present invention aims to provide a method whereby microspheres may be incorporated in a polyolefin matrix to form a composite material which can be employed in rigorous application areas, for example as an insulating casing for an underwater flowline, and wherein the properties of the composite material may be closely controlled.

In accordance with the present invention there is provided a method for the preparation of a composite material comprising a polyolefin selected from polypropylene and a polybutylene, and a filler comprising hollow microspheres, the method comprising:

- treating at least some of the microspheres to be incorporated in the polyolefin with a compound which acts as a chain-scission agent for the polyolefin;
- providing an even distribution of said microspheres in said polyolefin in its melt phase, and
- forming the composite material into a desired shape and cooling.

By means of the present invention, accurate control of the Melt Flow Index of the composite material may be achieved. It is found that the method of the present invention enables composite materials to be produced which meet the onerous requirements of use as flowline insulation materials, being of suitable Melt Flow Index for pipeline extrusion, without causing an unacceptable degree of microsphere breakage.

By means of a chain-scission agent, which acts to form free radicals in the polyolefin melt, and which is carried to the polyolefin by the microspheres, accurate control of mechanical properties, for example yield strength, extensibility to break and creep resistance, are obtainable. The composite material may be "tailored" to the requirements of the particular application area by selection of the base polyolefin and/or the type and quantity of the chain-scission agent. Further "tailoring" may be achievable by use of one or more functionalizing agents which act to graft polar functions onto the polymer chain, and thereby enable the polypropylene to "wet" the microspheres. This has the effect of improving yield strength and creep resistance. Examples of suitable functionalizing agents which act to graft polar functions onto the polymer chain are carboxylating agents, for example azidosulphonyl benzoic acid, or, preferably, an unsaturated

organic acid or anhydride, for example itaconic acid or maleic anhydride. Such a functionalizing agent may suitably be present in an amount of from 0.1 to 5 wt% (on base polyolefin). Preferably a functionalizing agent, when present, is also carried into the polyolefin on the microspheres.

A preferred chain-scission agent for use in the present invention is an azonitrile or, especially, an organic peroxide.

Suitable organic peroxides may include those of the aliphatic hydrocarbon, aromatic hydrocarbon, carboxylic acid ester, ketone, or carbonic acid ester types, and specific examples include diisopropyl peroxide, tertiary butyl peroxide, tertiary butyl hydroperoxide, dicumyl peroxide, dibenzoyl peroxide, cumyl hydroperoxide, tertiary butyl peracetate, tertiary butyl peroxy laurate, tertiary butyl perbenzoate, tertiary butyl perphthalate, methylethylketone peroxide, octanol peroxide, and diisopropyl peroxy carbonate. An especially preferred peroxide is DHBP (2,5-dimethyl-2,5-di(tertiary butyl peroxy)hexane or 2,5-dimethyl-2,5-di(tertiary butyl peroxy)hexyne-3. Examples of the azonitrile are azobisisopropionitrile and azobisisobutyronitrile.

A chain-scission agent may suitably be present in an amount of from 0.001 to 0.5 wt%, preferably from 0.005 to 0.1 wt%, and most preferably, from 0.01 to 0.06 wt%, based on weight of base polyolefin. A chain-scission agent is employed to cause a narrowing of the molecular weight distribution of the polyolefin.

The chain-scission agent may be added to the microsphere sample which is to be incorporated in the composite material, and mixed. However, it will be noted from the foregoing paragraph that the quantity of the chain-scission agent may be very small. It will also be appreciated that the volume of the light microspheres may be very large. Even distribution of the chain-scission agent can be difficult to achieve. It has been found to be beneficial for the achievement of good mixing to make a "master mix" of the chain-scission agent and a relatively small volume of microspheres, and to mix this with a relatively large volume, for example at least ten times the volume of uncoated microspheres. The achievement of an even distribution of chain-scission agent throughout the microspheres, by means of this method, is therefore a preferred step in the present invention.

A similar "master mix" method may be employed in relation to a functionalizing agent, as hereinbefore described, when such is employed. To prepare a microsphere sample for compounding, a final "master mix" may first be prepared by mixing together the chain-scission agent "master mix" and the functionalizing agent "master mix". Alternatively, the two "master mixes" may be separately added to uncoated microspheres. Alternatively a chain-scission agent and a functionalizing agent may be mixed, and then used to prepare a "master mix".

Distribution may be aided by diluting the chain-scission reagent (and/or a functionalizing agent, when employed) in a suitable solvent, which solvent is later removed by evaporation. Obviously, a solvent should be selected, which has substantially greater volatility than the chain-scission agent, or the functionalizing agent, when present.

The polypropylene or polybutylene used in this invention may be a homo- or a copolymer. Suitable copolymers are those comprising from 5 to 20 %wt of ethylene as comonomer. The homo- or copolymers may be employed in the form of blends with other polymers, such blends then comprising 1-50 wt%, preferably 10-40 wt% of other polymers such as polyamides and thermoplastic elastomers, e.g. those sold under the Trade Mark KRATON, and EPDM rubbers.

Suitably, the Melt Flow Index of base polymers (whether homo-, co- or terpolymers) may be in the range 0.5-60, preferably 2-20, most preferably 3-10 gms/10 min (per ISO 1133).

A preferred polyolefin for use in the present invention is based on polypropylene. A polybutylene material, when employed, is preferably based on butene-1.

The filler may comprise hollow microspheres substantially alone, or in combination with other filler materials, including non-hollow filler materials, for example talc, chalk, barium carbonate or chopped glass fibres. Preferably, however, the filler substantially consists of hollow microspheres (although in interpreting this statement it should be noted that any given sample of microspheres may contain a minor proportion of broken or solid microspheres).

In accordance with the present invention the microspheres carrying a chain-scission agent may be mixed with the polyolefin in particulate form and the material heated, to melt the polyolefin. Preferably, however, the microspheres are added to the polyolefin in its melt phase.

Preferably, the microspheres are present in the composite material in an amount of from 5 to 70%, preferably 30 to 60%, most preferably 40-55% by volume, on volume of the composite material.

Microspheres may be made of various plastics and inorganic materials. A preferred material is an inorganic glass, preferably a silica-based glass. A particular preferred material may comprise a major proportion of silica and minor proportions of an alkali metal oxide and  $B_2O_3$ .

The bulk density of the microspheres may suitably be in the range 0.07-0.6 g/ml, preferably 0.35-0.5

g/ml. The diameter of the microspheres may typically be in the range 10 to 200  $\mu\text{m}$ , preferably 20 to 130  $\mu\text{m}$ . The isostatic compressive strength may be in the range 1000-25000 p.s.i. ( $6.9 \times 10^6 \text{ Pa}$  -  $1.03 \times 10^8 \text{ Pa}$ ), preferably in the range 5000-15000 p.s.i. ( $3.4 \times 10^7 \text{ Pa}$  -  $1.03 \times 10^8 \text{ Pa}$ ).

Preferably, a method in accordance with the present invention produces a composite material having a

5 Melt Flow Index of 0.5-20, preferably 0.5-3, most preferably 1-2. Preferably it has a relative density in the range 0.4-0.85, preferably 0.65 - 0.75.

The polyolefin desirably contains an antioxidant.

In accordance with another aspect of the present invention there is provided a composite material prepared in accordance with a method as previously described. The material may be provided as tapes or, 10 preferably, pellets, for use in a later injection moulding or extrusion process. Alternatively, a sheet of the composite material could be produced, for use in a later compression moulding or thermoforming process.

Said material may be suitable for use as a flowline insulation composition and further aspects of the invention relate to such a composition, and to a method of forming a flowline insulation layer comprising the step of extruding composite material as hereinbefore described, onto a steel pipe. If desired the contact 15 between the composite material and the steel pipe may be improved by means of a carboxylated polyolefin layer therebetween. It is possible moreover, because of the excellent mechanical properties and suitable Melt Flow Index which can be achieved in such a composite material, that it may serve as the self-supporting load-bearing wall of a flowline, rather than as an insulating composition on a load-bearing steel pipe.

20 The composite material can be extruded in the form of tapes and applied to a steel pipe by wrapping around a steel pipe, suitably as the pipe rotates. This method is known as "side wrapping". A preferred method to apply the material to a steel pipe is by extruding it in the form of a shell, around a steel pipe. This method is known as "pipe extrusion" because the extrusion of the polymer material is in the shape of a pipe. Pipe extrusion is a difficult, high shear, process requiring a material of low Melt Flow Index; but a 25 desired casing thickness of about 4-60 mm may be achieved in a single step using composite materials of the present invention. A preferred aspect of the present invention therefore relates to a method of preparing an insulated flowline by applying a composite material of the present invention to a steel pipe by a "pipe extrusion" method. If additional layers are required a co-extrusion process may be employed.

A composite material as hereinbefore described may find application in areas other than flowline 30 insulation. For example it could be of use in refrigeration equipment, buoyancy aids, aerospace equipment, or land vehicle applications, where its impact resistance and strength-to-weight ratio may be of greater interest than its thermal insulation property. It should be noted, therefore, that the composite materials of the present invention are not limited to the underwater flowline application area, nor is the method of the present invention limited to the production of materials which would have properties suitable therefor. The 35 method of the present invention enables the production of suitable materials therefor, which materials are of considerable interest, but also enables the production of materials of quite different properties, for different end uses, by permitting precise manipulation of properties to be achieved.

The invention will now be further described, by way of example.

40 1. General Procedures

Pre-treatment of microspheres with a peroxide

A master mix of 100 g hollow glass microspheres (for example hollow glass microspheres having a bulk 45 density in the range 0.17-0.49 g/ml and diameters in the range 20-130  $\mu\text{m}$ ) was produced by mixing the microspheres, in a 1 litre jar, with 0.3 g of a liquid peroxide, for example DHBP - 2,5-dimethyl-2,5-di(tertiary butyl peroxy)hexane - available under the Trade Mark INTEROX DHBP. After stirring for 10 minutes the "master mix" was added to a larger amount (for example 1-3 kg) of microspheres of the same type in a Henshal mixer, under a nitrogen blanket, and mixed for 10 minutes, until even distribution was achieved.

50 The microspheres may if desired be subjected to an initial test to assess the proportion of undesirable constituents therein, namely broken microspheres and solid or near-solid microspheres. A simple flotation test may be employed, whereby a test sample is placed in a liquid, conveniently water, and the proportion of particles which sink is assessed against those which float. If the assessment is that there is an undesirably high proportion of non-buoyant particles in the test sample, the same technique may be used 55 on all of the microspheres to be incorporated in the composite material, to remove substantially all non-buoyant particles.

In some embodiments it may be desired to dilute the peroxide in a solvent, which has a substantially greater volatility than the peroxide. The solvent evaporates during the step of mixing the master mix with

EP 0 473 215 A1

uncoated microspheres, under reduced pressure if required, or by purging, for example with nitrogen.

In another embodiment a master mix is not prepared. The peroxide is simply mixed with a large volume of microspheres in a Henshal mixer until an even distribution of peroxide is obtained.

6 Pre-treatment of microspheres with a peroxide and maleic anhydride

A master mix of peroxide-coated microspheres is prepared, as described above. A separate master mix of microspheres coated with maleic anhydride is prepared, typically in such an amount as to introduce approximately 0.5 wt% maleic anhydride (on weight polyolefin) into the polyolefin. The maleic anhydride 10 may be dissolved in a minimum amount of methanol, subsequently removed by purging with nitrogen. A desired quantity of each said master mix may be mixed together to provide the final master mix which may be mixed with a larger volume of uncoated microspheres.

Compounding

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Using a Baker-Perkins twin screw compounding extruder MP 2030, pellets of polypropylene (homo- or copolymer) were fed to the main feed port at a rate of 5 kg/hour. The extrusion temperature was kept at 200 °C and the screw speed was 200 rpm. The treated microspheres were fed into the polypropylene melt using a side feeder at a rate of 2.3 kg/hour, the microspheres constituting about 40-55% by volume of the 20 composite material. The composite material was extruded and pelletized.

Test Procedures		
25	Melt Flow Index (MFI)	ISO 1133
	Density	ISO 1183
	Flexural strength	ASTM D790
	Flexural strain at yield	ASTM D790
	Tensile strength at break	ISO 527
	Tensile elongation at break	ISO 527
30	Tensile strength at yield	ISO 527
	Tensile elongation at yield	ISO 527
	Water Absorption	ASTM C272-53
	Thermal conductivity	BS 874
35	Dimensional stability	ISO 2796

2. Examples, Results and Discussion - Set 1

40 In this set of Examples a polypropylene copolymerized with 10 wt% ethylene (on total polymer weight), and having a Melt Flow Index of 4, was compounded with

(A) uncoated microspheres;

(B) microspheres carrying 0.038 wt% DHBP (on wt. microspheres; approximately 0.02 wt% on polymer in the composite material);

(C) microspheres carrying 0.045 wt% DHBP (on wt. microspheres); and

(D) a polypropylene copolymerized during the polymerization reaction with 10 wt% ethylene (on total polymer weight), and having a Melt Flow Index of 19, was compounded with uncoated microspheres.

In each case the microspheres made up 50% by volume of the composite material.

The pellets of the composite materials were injection moulded into test pieces for evaluation of their properties.

50 The results are presented in Table 1, from which it will be seen that compounding uncoated microspheres with the polypropylene of Melt Flow Index 4, result (A), produced a composite material of MFI 0.07. Elongation at break is very high. However, the composite material was discoloured and had a density of 0.85 g/ml. "Ashing" of the composite material - placing it in an oven at 550 °C to fully remove the polypropylene to leave the filler - enabled the filler to be analysed, by the flotation method as described above and by electron microscopy. This confirmed that a high proportion of microspheres had been broken. In conclusion, the low flow of the polypropylene melt is detrimental to the microspheres and the product is unsuitable for use as a flowline insulation material.

Compounding uncoated microspheres with polypropylene of Melt Flow Index 19, result (D), enabled

EP 0 473 215 A1

microspheres to be incorporated without breakage, producing a composite material with a density of 0.7 g/ml. However, the MFI, at 3.5, is too high for pipe extrusion. Moreover the elongation at break is reduced to 8% due to the reduced molecular weight of the base polymer.

It will be seen from Table 1 that application of very small quantities of the peroxide to the microspheres, 6 results (B) and (C), enabled the microspheres to be compounded with polypropylene with the relatively low Melt Flow Index of 4 and produced composite material suitable as a flowline insulation material. The density of the materials produced was 0.7 g/ml, indicating little microsphere breakage. This was further confirmed by "ashing" followed by flotation and electron microscopy analysis. Tensile strength and flexural properties were maintained and tensile elongation at break was good, particularly for the example using the lower 10 amount of peroxide. They were the only materials with a suitable balance of properties for use as a flowline insulation material and application by pipe extrusion.

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TABLE 1

TENSILE      TENSILE      FLEXURAL

Compounded Material	MFI (g/10 min)	Dens. (g/ml)	Yield Stress MPa	Strength at break MPa	Strain at break %	Strength MPa	Strain at Yield %
A) PPCO (MFI 4) + 50v% ms	0.07	0.85	10.2	3.7	9.8	32	18.2
B) PPCO (MFI 4) + 50v% ms + 0.038 perox.)	1.5	0.7	10.8	0.74	9.0	25.7	17.8
C) PPCO (MFI 4) + (50v% ms + 0.045% perox.)	1.7	0.7	11.1	0.72	9.3	13.0	19.0
D) PPCO (MFI 19) + 50v% ms	3.5	0.7	9.8	0.50	8.4	8.4	17.4

Materials in accordance with the invention, as described above, have been tested in respect of their thermal conductivity, water absorption, and dimensional stability at 70 °C. The results are as follows:

Thermal conductivity      0.14 W/mK

Water absorption      0.06%

Dimensional stability (70 °C)      0.2%

The results further confirm the suitability of these materials as flowline insulation materials.

Examples, Results and Discussion - Set 2

5 A polypropylene homopolymer of Melt Flow Index 11 was compounded with  
 a) uncoated microspheres of density 0.38 g/cc and  
 b) such microspheres carrying peroxide (0.02 wt% on polypropylene) and maleic anhydride (MALA - 0.5  
 wt% on polypropylene).

10 The results are shown in Table 2.

TABLE 2

15 <u>Property</u>	PP + ms	PP + (ms + perox. + MALA)
MFI (g/10 min)	1.5	1.7
microsphere content 20 (wt% on composite material)	29.5	28.6
Density (g/ml)	0.706	0.685
Tensile strength 25 at yield (MPa)	10.4	16.0
Elongation at yield (%)	3	0.7
Tensile strength 30 at break (MPa)	10.0	16.1
Elongation at break (%)	70	3

It will be observed from Table 2 that the use of a small amount of peroxide and maleic anhydride 35 causes substantial changes in the properties of the composite material. Tensile strength is substantially enhanced whilst a Melt Flow Index suitable for pipe extrusion is maintained. Adhesion between microspheres and polymers is believed to be improved thereby increasing creep resistance. The maleic anhydride is thought to improve the adhesion between the microspheres and the polymer by introduction of carboxyl groups on the latter. The material is suitable for many uses, including flowline insulation when the 40 flowline is to be installed by a method causing less strain on the flowline than reel barging. The properties could be modified by adjustment of the concentrations of the peroxide and/or the maleic anhydride. Reduction of the amount of maleic anhydride would be expected to cause an increase in the elongation at break of the composite material and so enable a composite material suitable for installation by reel barging to be produced.

45 **Claims**

1. A method for the preparation of a composite material comprising a polyolefin selected from polypropylene and a polybutylene, and a filler comprising hollow microspheres, the method comprising:  
 50     - treating at least some of the microspheres to be incorporated in the polyolefin with a reagent which acts as a chain-scission agent for the polyolefin;  
 - providing an even distribution of said microspheres in said polyolefin in its melt phase; and  
 - forming the composite material into a desired shape and cooling.
- 65 2. A method as claimed in claim 1, wherein the microspheres are made of an inorganic glass.
3. A method as claimed in any claim 1 or 2, wherein the chain-scission agent is an organic peroxide.

4. A method as claimed in claim 3 wherein the organic peroxide is present in an amount of 0.001 to 0.5 wt% based on weight of polyolefin.
5. A method as claimed in any preceding claim, wherein the microspheres to be incorporated in the polyolefin are treated with a chain-scission agent by
  - preparing a sample of microspheres by treatment thereof with a chain-scission agent, such that the concentration of chain-scission agent on the microspheres is higher than is required for compounding, and
  - diluting the treated sample or a portion thereof with microspheres which have not been treated with the chain-scission agent.
- 10 6. A method as claimed in any preceding claim, comprising the step of additionally treating at least some of the microspheres to be incorporated into the polyolefin with an azidosulphonylbenzoic acid or an unsaturated organic acid or anhydride.
- 15 7. A method as claimed in any preceding claim, wherein the composite material produced has a Melt Flow Index in the range 0.5-5 g/10 min and a density in the range 0.65-0.75 g/ml.
- 20 8. A method of forming a flowline having an insulating layer which method comprises the step of extruding composite material, prepared by a method as claimed in any one of claims 1 to 7 onto a steel pipe.
- 25 9. A method of forming a shaped article, comprising:
  - preparing a composite material in particulate form, by a method as claimed in any of claims 1 to 7;
  - melting a required amount of said composite material, and
  - forming said shaped article by extrusion or injection moulding.

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## EUROPEAN SEARCH REPORT

Application Number

EP 91 20 1997

### DOCUMENTS CONSIDERED TO BE RELEVANT

Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int. CL.5)
D, A	DE-A-2 445 075 (FUJIKURA CABLE WORKS) * page 4, line 19 - line 24 * * page 5, line 10 - line 13 * * page 6, line 10 - line 14 * * page 8, line 3 - line 14 * * page 13 - page 14; example 3 * * claims 1-3,5-6 * ---	1	C08K9/04 C08K7/22 C08L23/12 C08L 23/20
A	FR-A-2 102 270 (PPG INDUSTRIES) * claim 1 * ---	1,3-4	
A	GB-A-1 514 716 (CHLORIDE GROUP LTD) * page 1, line 29 - line 33 * * page 2; examples 2-6 * * claims 1-2,5 *	1	
-----			TECHNICAL FIELDS SEARCHED (Int. CL.5 )
			C08K C08L
The present search report has been drawn up for all claims			
Place of search	Date of completion of the search	Examiner	
THE HAGUE	20 NOVEMBER 1991	SIEMENS T.	
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